

# LTC7897

Datasheet Comparison



Updated gate drive ABS MAX rating under FEATURES and GENERAL DESCRIPTION sections

#### **Before**

140V, Low I<sub>0</sub>, Synchronous Buck Controller with Programmable 5V to 10V Gate Drive

#### **FEATURES**

- ► Wide V<sub>IN</sub> Range: 4V to 135V (140V ABS MAX)
- Wide Output Voltage Range: 0.8V ≤ V<sub>OUT</sub> ≤ 135V (140V ABS MAX)
- Adjustable Gate Drive Level: 5V to 10V (OPTI-DRIVE, 15V ABS MAX)
- ► Adjustable Driver Voltage UVLO
- ► Adaptive or Resistor Adjustable Dead Times
- Split-Output Gate Drivers for Adjustable Turn-On and Turn-Off Driver Strengths
- ► 100% Duty Cycle Operation
- Low Operating I<sub>O</sub>: 5μA (48V<sub>IN</sub> to 3.3V<sub>OUT</sub>)
- ► Spread Spectrum Frequency Modulation
- ► Programmable Frequency (100kHz to 2.5MHz)
- ► Synchronizable Frequency (100kHz to 2.5MHz)
- ▶ 28-Pin (4mm x 5mm) QFN Package

#### APPLICATIONS

- ► Industrial Power Systems
- Military/Avionics
- ► Telecommunications Power Systems

#### **GENERAL DESCRIPTION**

The LTC°7897 is a high performance, 100% duty cycle capable, synchronous step-down, DC/DC switching regulator controller that drives all N-channel synchronous silicon metal oxide field effect transistor (MOSFET) power stages. Synchronous rectification increases efficiency, reduces power loss, and simplifies the application design by reducing thermal requirements.

The wide input and output voltage ranges of the LTC7897 enable not only high step-down ratios but also a wide range of positive to negative voltage conversion.

The gate drivers of the LTC7897 provide robustness with a 15V ABS MAX rating and flexibility with adjustable drive levels and dead times to optimize applications. The gate drive voltage of the LTC7897 can optionally be adjusted from 5V to 10V to allow use of logic-level or standard threshold MOSFETs. The dead times of the LTC7897 can be optimized with external resistors for margin or to tailor the application for higher efficiency and allow for high frequency operation.

#### **After**

140V, Low I<sub>0</sub>, Synchronous Buck Controller with Programmable 5V to 10V Gate Drive

Techdoc: change from 15V to 14V

#### FEATURES

- ► Wide V<sub>IN</sub> Range: 4V to 135V (140V ABS MAX)
- Wide Output Voltage Range: 0.8V ≤ V<sub>OUT</sub> ≤ 135V (140V ABS MAX)
- Adjustable Gate Drive Level: 5V to 10V (OPTI-DRIVE,
- 14V (15V) ABS MAX)
  - ► Adjustable Driver Voltage UVLO
  - ► Adaptive or Resistor Adjustable Dead Times
  - ► Split-Output Gate Drivers for Adjustable Turn-On and Turn-Off Driver Strengths
  - ► 100% Duty Cycle Operation
  - Low Operating I<sub>Q</sub>: 5μA (48V<sub>IN</sub> to 3.3V<sub>OUT</sub>)
  - ► Spread Spectrum Frequency Modulation
  - ► Programmable Frequency (100kHz to 2.5MHz)
  - ► Synchronizable Frequency (100kHz to 2.5MHz)
  - ► 28-Pin (4mm x 5mm) QFN Package

#### **APPLICATIONS**

- ► Industrial Power Systems
- Military/Avionics
- ► Telecommunications Power Systems

#### GENERAL DESCRIPTION

The LTC\*7897 is a high performance, 100% duty cycle capable, synchronous step-down, DC/DC switching regulator controller that drives all N-channel synchronous silicon metal oxide field effect transistor (MOSFET) power stages. Synchronous rectification increases efficiency, reduces power loss, and simplifies the application design by reducing thermal requirements.

The wide input and output voltage ranges of the LTC7897 enable not only high step-down ratios but also a wide range of positive to negative voltage conversion.

The gate drivers of the LTC7897 provide robustness with 14V (15V) ABS MAX rating and flexibility with adjustable drive levels and dead times to optimize applications. The gate drive voltage of the LTC7897 can optionally be adjusted from 5V to 10V to allow use of logic-level or standard threshold MOSFETs. The dead times of the LTC7897 can be optimized with external resistors for margin or to tailor the application for higher efficiency and allow for high frequency operation.



► Correct text format.

## **Before**

A	6/25	Updated Features and General Description sections	1
		Specifications and Absolute Maximum Ratings sections	4-9
		Updated Pin Descriptions table	11
		Updated Figure 4, Figure 23, Figure 25, and Figure 30	14, 18, 19
		Updated DRV <sub>cc</sub> and INTV <sub>cc</sub> Regulators (OPTI-DRIVE) section	37
		Updated Minimum On-Time Considerations section	38
		Updated Efficiency Considerations section	40
		Updated Figure 54 and Figure 58	46, 48

REVISION NUMBER	REVISION DATE	DESCRIPTION	PAGE NUMBER
0	2/25	Initial release	_
A	6/25	Updated Features and General Description sections Specifications and Absolute Maximum Ratings sections Updated Pin Descriptions table Updated Figure 4, Figure 23, Figure 25, and Figure30 Updated DRV <sub>Cc</sub> and INTV <sub>Cc</sub> Regulators (OPTI-DRIVE) Section Updated Minimum On-Time Considerations section Updated Efficiency Considerations section Updated Figure 54 and Figure 58	1 4-9 11 14, 18, 19 37 38 40 46, 48



Corrected DRVSET condition setting

#### **Before**

Data Sheet LTC7897

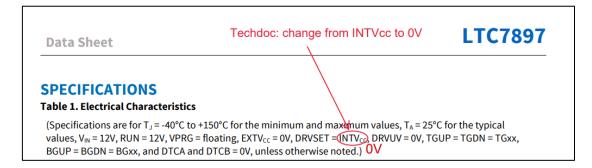
#### **SPECIFICATIONS**

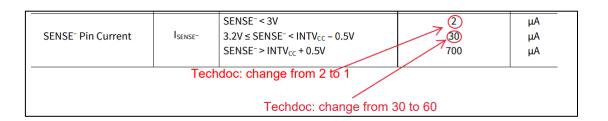
#### **Table 1. Electrical Characteristics**

(Specifications are for  $T_J$  = -40°C to +150°C for the minimum and maximum values,  $T_A$  = 25°C for the typical values,  $V_{IN}$  = 12V, RUN = 12V, VPRG = floating, EXTV<sub>CC</sub> = 0V, DRVSET = INTV<sub>CC</sub>, DRVUV = 0V, TGUP = TGDN = TGxx, BGUP = BGDN = BGxx, and DTCA and DTCB = 0V, unless otherwise noted.)

Updated typical value on Sense- Pin Current

		SENSE <sup>-</sup> < 3V	2	μΑ
SENSE <sup>-</sup> Pin Current	I <sub>SENSE</sub> -	$3.2V \le SENSE^- < INTV_{CC} - 0.5V$	30	μΑ
		SENSE <sup>-</sup> > INTV <sub>CC</sub> + 0.5V	700	μΑ



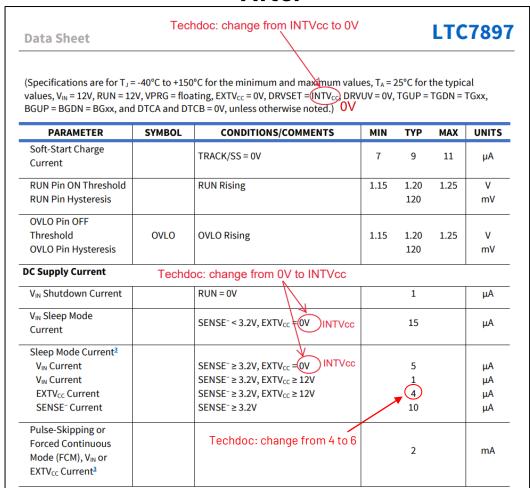




► Corrected DRVSET and EXTVcc conditions setting and updated typical value on EXTVcc current

#### **Before**

Specifications are for T <sub>J</sub> =	40°C to :15					
		0°C for the minimum and mavimum va	dues T = '	DE°C for	the tunic	al.
		ating, EXTV <sub>CC</sub> = 0V, DRVSET = INTV <sub>CC</sub> , D				
	•	TCB = 0V, unless otherwise noted.)			. 05.1	· Ozz,
PARAMETER	SYMBOL	CONDITIONS/COMMENTS	MIN	TYP	MAX	UNITS
Soft-Start Charge						
Current		TRACK/SS = 0V	7	9	11	μA
RUN Pin ON Threshold		RUN Rising	1.15	1.20	1.25	V
RUN Pin Hysteresis				120		mV
OVLO Pin OFF						
Threshold	OVLO	OVLO Rising	1.15	1.20	1.25	V
OVLO Pin Hysteresis				120		mV
C Supply Current						
V <sub>IN</sub> Shutdown Current		RUN = 0V		1		μА
V <sub>IN</sub> Sleep Mode		CENCE- 12 2W EVTV - OV		15		
Current		SENSE <sup>-</sup> < 3.2V, EXTV <sub>CC</sub> = 0V		15		μΑ
Sleep Mode Current <sup>3</sup>						
V <sub>IN</sub> Current		SENSE <sup>-</sup> $\geq$ 3.2V, EXTV <sub>CC</sub> = 0V		5		μA
V <sub>IN</sub> Current		SENSE <sup>-</sup> ≥ 3.2V, EXTV <sub>CC</sub> ≥ 12V		1		μA
EXTV <sub>CC</sub> Current		SENSE <sup>-</sup> $\geq$ 3.2V, EXTV <sub>CC</sub> $\geq$ 12V		4		μA
SENSE <sup>-</sup> Current		SENSE⁻≥3.2V		10		μА
Pulse-Skipping or						
Forced Continuous		I				

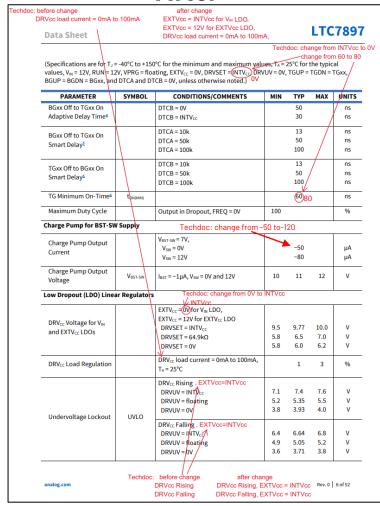




 Corrected DRVSET and EXTVcc conditions setting. Updated TG Minimum On-Time typical value and Charge pump output current

#### **Before**

alues, V <sub>IN</sub> = 12V, RUN = 12	V, VPRG = flo	$0^{\circ}$ C for the minimum and maximum valuating, EXTV <sub>cc</sub> = 0V, DRVSET = INTV <sub>cc</sub> , DRV TCB = 0V, unless otherwise noted.)				
PARAMETER	SYMBOL	CONDITIONS/COMMENTS	MIN	TYP	MAX	UNITS
BGxx Off to TGxx On Adaptive Delay Time <sup>4</sup>		DTCB = 0V DTCB = INTVcc		50 30		ns ns
Adaptive Delay Tilles						
BGxx Off to TGxx On		DTCA = 10k		13		ns
Smart Delay⁵		DTCA = 50k DTCA = 100k		50 100		ns ns
		DTCA = 100K				ns
TGxx Off to BGxx On		DTCB = 10k		13		ns
Smart Delay <sup>5</sup>		DTCB = 50k		50		ns
		DTCB = 100k		100		ns
TG Minimum On-Time <sup>s</sup>	ton(MIN)			60		ns
Maximum Duty Cycle		Output in Dropout, FREQ = 0V	100			%
harge Pump for BST-SW	Supply	I				I
Charge Pump Output		$V_{BST-SW} = 7V$ ,				
Current		V <sub>SW</sub> = 0V		-50		μΑ
		V <sub>SW</sub> = 12V		-80		μA
Charge Pump Output Voltage	$V_{\text{BST-SW}}$	$I_{BST} = -1\mu A$ , $V_{SW} = 0V$ and $12V$	10	11	12	٧
ow Dropout (LDO) Linea	r Regulator	•				
		EXTV <sub>CC</sub> = 0V for V <sub>IN</sub> LDO, EXTV <sub>CC</sub> = 12V for EXTV <sub>CC</sub> LDO				
DRV <sub>CC</sub> Voltage for V <sub>IN</sub>		DRVSET = INTVcc	9.5	9.77	10.0	v
and EXTV <sub>CC</sub> LDOs		DRVSET = 64.9kΩ	5.8	6.5	7.0	v
		DRVSET = 0V	5.8	6.0	6.2	V
DRV <sub>cc</sub> Load Regulation		DRV <sub>CC</sub> load current = 0mA to 100mA, T <sub>A</sub> = 25°C		1	3	%
		DRV <sub>cc</sub> Rising				
		DRVUV = INTV <sub>CC</sub>	7.1	7.4	7.6	V
		DRVUV = floating	5.2	5.35	5.5 4.0	V
Undervoltage Lockout	UVLO	DRVUV = 0V	3.8	3.93	4.0	V
-		DRV <sub>cc</sub> Falling				
		DRVUV = INTV <sub>CC</sub>	6.4 4.9	6.64 5.05	6.8 5.2	V
		DRVUV = floating DRVUV = 0V	3.6	3.71	3.8	V





► Corrected DRVSET condition setting. Updated max value on EXTVcc Rising.

#### **Before**

After

Data Sheet LTC7897

(Specifications are for  $T_J = -40$ °C to +150°C for the minimum and maximum values,  $T_A = 25$ °C for the typical values,  $V_{IN} = 12V$ , RUN = 12V, VPRG = floating, EXTV<sub>CC</sub> = 0V, DRVSET = INTV<sub>CC</sub>, DRVUV = 0V, TGUP = TGDN = TGxx, BGUP = BGDN = BGxx, and DTCA and DTCB = 0V, unless otherwise noted.)

Techdoc: change from INTVcc to 0V

Data Sheet

Techdoc: change from INTVcc to 0V

LTC7897

(Specifications are for  $T_J = -40^{\circ}\text{C}$  to +150°C for the minimum and maximum values,  $T_A = 25^{\circ}\text{C}$  for the typical values,  $V_{IN} = 12V$ , RUN = 12V, VPRG = floating, EXTV<sub>CC</sub> = 0V, DRVSET =  $(NTV_{CC})$ DRVUV = 0V, TGUP = TGDN = TGxx, BGUP = BGDN = BGxx, and DTCA and DTCB = 0V, unless otherwise noted.) 0V

Data Sheet LTC7897

(Specifications are for  $T_J = -40^{\circ}\text{C}$  to +150°C for the minimum and maximum values,  $T_A = 25^{\circ}\text{C}$  for the typical values,  $V_{IN} = 12\text{V}$ , RUN = 12V, VPRG = floating, EXTV<sub>CC</sub> = 0V, DRVSET = 0V, DRVUV = 0V, TGUP = TGDN = TGxx, BGUP = BGDN = BGxx, and DTCA and DTCB = 0V, unless otherwise noted.)

PARAMETER	SYMBOL	CONDITIONS/COMMENTS	MIN	TYP	MAX	UNITS
EXTV <sub>CC</sub> LDO		DRVUV = INTV <sub>CC</sub> , $T_A = 25$ °C	7.5	7.7	8.0	V
Switchover Voltage		DRVUV = floating, T <sub>A</sub> = 25°C	5.9	6.1	6.4	V
EXTV <sub>cc</sub> Rising		DRVUV = 0V, $T_A = 25$ °C	4.6	4.8	5.0	V

Techdoc: Change from 5.0 to 5.1 LTC7897 **Data Sheet** (Specifications are for  $T_1 = -40^{\circ}$ C to +150°C for the minimum and maximum values,  $T_A = 25^{\circ}$ C for the typical values,  $V_{IN} = 12V$ , RUN = 12V, VPRG = floating, EXTV<sub>CC</sub> = 0V, DRVSET = 0V, DRVUV = 0V, TGUP = TGDN = TGxx, BGUP = BGDN = BGxx, and DTCA and DTCB = 0V, unless otherwise noted.) TYP PARAMETER SYMBOL CONDITIONS/COMMENTS MIN MAX UNITS EXTV<sub>CC</sub> LDO DRVUV = INTV<sub>CC</sub>,  $T_A = 25$ °C 7.5 7.7 8.0 DRVUV = floating,  $T_A = 25^{\circ}C$ 5.9 Switchover Voltage 6.1 DRVUV = 0V,  $T_A = 25$ °C EXTV<sub>cc</sub> Rising 4.6 4.8



Corrected DRVSET condition setting.

**Before** 

After

Data Sheet LTC7897

(Specifications are for  $T_J = -40$ °C to +150°C for the minimum and maximum values,  $T_A = 25$ °C for the typical values,  $V_{IN} = 12V$ , RUN = 12V, VPRG = floating, EXTV<sub>CC</sub> = 0V, DRVSET = INTV<sub>CC</sub>, DRVUV = 0V, TGUP = TGDN = TGxx, BGUP = BGDN = BGxx, and DTCA and DTCB = 0V, unless otherwise noted.)

Techdoc: change from INTVcc to 0V LTC7897

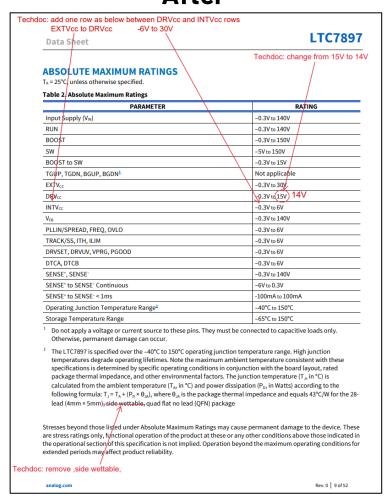
(Specifications are for  $T_J = -40^{\circ}\text{C}$  to  $+150^{\circ}\text{C}$  for the minimum and maximum values,  $T_A = 25^{\circ}\text{C}$  for the typical values,  $V_{IN} = 12V$ , RUN = 12V, PRG = floating,  $EXTV_{CC} = 0V$ ,  $PRVSET = \text{INTV}_{CC}$ , PRVUV = 0V, PRUV = TGDN = TGXX, PRUV = TGX



▶ Updated DRVcc ABS MAX rating. Added EXTVcc to DRVcc ABS MAX rating. Removed side wettable description under Note 2.

#### **Before**

RATING  -0.3V to 140V  -0.3V to 140V  -0.3V to 150V  -5V to 150V  -0.3V to 15V  Not applicable  -0.3V to 30V  -0.3V to 15V  -0.3V to 6V
-0.3V to 140V -0.3V to 140V -0.3V to 150V -5V to 150V -0.3V to 15V Not applicable -0.3V to 30V -0.3V to 15V -0.3V to 6V
-0.3V to 150V -5V to 150V -0.3V to 15V Not applicable -0.3V to 30V -0.3V to 15V -0.3V to 6V
-5V to 150V -0.3V to 15V Not applicable -0.3V to 30V -0.3V to 15V -0.3V to 6V
-0.3V to 15V Not applicable -0.3V to 30V -0.3V to 15V -0.3V to 6V
Not applicable -0.3V to 30V -0.3V to 15V -0.3V to 6V
-0.3V to 30V -0.3V to 15V -0.3V to 6V
-0.3V to 15V -0.3V to 6V
-0.3V to 6V
-0.3V to 140V
-0.3V to 6V
-0.3V to 140V
-6V to 0.3V
-100mA to 100mA
-40°C to 150°C
-65°C to 150°C
nected to capacitive loads only.  Derature range. High junction  temperature consistent with these  ton with the board layout, rated  tion temperature (T <sub>p.</sub> in °C) is  no (P <sub>p.</sub> in Wats) according to the  spedance and equals 43°C/W for the 28
oermanent damage to the device. Thes ther conditions above those indicated i the maximum operating conditions fo





Updated pin description for EXTVcc

## **Before**

Data	Sheet	LTC789
		Connect VPRG to INTV $_{\rm CC}$ or GND to program the output to 12V or 5V, respectively, through an internal resistor divider on V $_{\rm FB}$ .
7	V <sub>IN</sub>	Main Supply Pin. A bypass capacitor must be tied between V <sub>IN</sub> and GND.
8	DRV <sub>cc</sub>	Gate Driver Output of the internal LDO regulator from $V_{IN}$ or EXTV <sub>CC</sub> . The gate drivers and the INTV <sub>CC</sub> internal LDO are powered from DRV <sub>CC</sub> . A low ESR 4.7 $\mu$ F ceramic bypass capacitor should be connected between DRV <sub>CC</sub> and GND, as close as possible to the IC.
9	OVLO	Overvoltage Lockout Input. A voltage on this pin above 1.2V disables switching of the controller. The $DRV_{CC}$ and $INTV_{CC}$ supplies maintain regulation during an OVLO event. Exceeding the OVLO threshold also triggers a soft-start reset. If the OVLO function is not used, connect this pin to GND.
10	EXTV <sub>cc</sub>	External Power Input to an Internal LDO Regulator Connected to DRV $_{CC}$ . This LDO regulator supplies INTV $_{CC}$ power, bypassing the internal V $_{IN}$ LDO regulator whenever EXTV $_{CC}$ is higher than the EXTV $_{CC}$ switchover voltage. See the EXTV $_{CC}$ connection in the <i>Power and Bias Supplies (VIN, EXTVCC, DRVCC, and INTVCC)</i> section. Do not exceed 30V on EXTV $_{CC}$ . Connect EXTV $_{CC}$ to GND if the EXTV $_{CC}$ LDO regulator is not used.

Techdoc: char	nge from GND	to INTVcc LTC7897
Data	Sheet	LICIOSI
		Connect VPRG to INTV <sub>CC</sub> or GND to program the output to 12V or 5V, respectively, through an internal resistor divider on $V_{\rm FB}$ .
7	V <sub>IN</sub>	Main Supply Pin. A bypass capacitor must be tied between V <sub>IN</sub> and GND.
8	DRV <sub>cc</sub>	Gate Driver Output of the internal LDO regulator from $V_{IN}$ or EXTV <sub>CC</sub> . The gate drivers and the INTV <sub>CC</sub> internal LDO are powered from DRV <sub>CC</sub> . A low ESR 4.7 $\mu$ F ceramic bypass capacitor should be connected between DRV <sub>CC</sub> and GND, as close as possible to the IC.
9	OVLO	Overvoltage Lockout Input. A voltage on this pin above 1.2V disables switching of the controller. The DRV <sub>CC</sub> and INTV <sub>CC</sub> supplies maintain regulation during an OVLO event. Exceeding the OVLO threshold also triggers a soft-start reset. If the OVLO function is not used, connect this pin to GND.
10	EXTV <sub>cc</sub>	External Power Input to an Internal LDO Regulator Connected to DRV <sub>CC</sub> . This LDO regulator supplies INTV <sub>CC</sub> power, bypassing the internal V <sub>IN</sub> LDO regulator whenever EXTV <sub>CC</sub> is higher than the EXTV <sub>CC</sub> switchover voltage. See the EXTV <sub>CC</sub> connection in the <i>Power and Bias Supplies (VIN, EXTVCC, DRVCC, and INTVCC)</i> section. Do not exceed 30V on EXTV <sub>CC</sub> . Connect EXTV <sub>CC</sub> to GND if the EXTV <sub>CC</sub> LDO regulator is not used.



Updated pin description for DRVSET

## **Before**

25	DTCA	Dead Time Control Pin for Bottom MOSFET Off to Top MOSFET On Delay. Connect DTCA to GND to program an adaptive delay of approximately 50ns. Connect DTCA to INTV $_{\text{CC}}$ to program an adaptive delay of approximately 30ns. Connect a $10k\Omega$ to $100k\Omega$ resistor between DTCA and GND to add a smart delay (from 13ns to 100ns) between BGUP falling and SW rising.
26	DRVSET	DRV $_{\rm CC}$ Regulation Program pin. This pin sets the regulation point for the DRV $_{\rm CC}$ low dropout (LDO) linear regulator. Connect to GND to set DRV $_{\rm CC}$ to 6.0V. Connect to INTV $_{\rm CC}$ to set DRV $_{\rm CC}$ to 10.0V. Program voltages between 5V and 10V by placing a resistor (50k to 100k) between DRVSET and GND. The resistor and an internal 20 $\mu$ A source current create a voltage used by the DRV $_{\rm CC}$ LDO regulator to set the regulation point.
27	DRVUV	DRV <sub>cc</sub> UVLO and EXTV <sub>cc</sub> Switchover Program Pin. DRVUV determines the DRV <sub>cc</sub> UVLO and EXTV <sub>cc</sub> switchover rising and falling thresholds, as listed in <i>Table 1</i> .
28	RUN	Run Control Input for the Controller. Forcing the RUN pin below 1.1V disables control, while forcing the RUN pin below 0.7V shuts down the entire LTC7897, reducing quiescent current to approximately 1 $\mu$ A. Tie the RUN pin to V $_{\text{IN}}$ for always-on operation.
29	GND (EPAD)	Ground (Exposed Pad). The exposed pad must be soldered to PCB GND for rated electrical and thermal performance.
analog.co	om	Rev. A   12 of 52

## **After**

DRVSET	DRV $_{CC}$ Regulation Program pin. This pin sets the regulation point for the DRV $_{CC}$ low dropout (LDO) linear regulator. Connect to GND to set DRV $_{CC}$ to 6.0V. Connect to INTV $_{CC}$ to set DRV $_{CC}$ to 10.0V. Program voltages between 5V and 10V by placing a resistor (50k to 100k) between DRVSET and GND. The resistor and an internal 20 $\mu$ A source current create a voltage used by the DRV $_{CC}$ LDO regulator to set the regulation point.
DRVUV	$DRV_{CC}$ UVLO and EXTV <sub>CC</sub> Switchover Program Pin. DRVUV determines the DRV <sub>CC</sub> UVLO and EXTV <sub>CC</sub> switchover rising and falling thresholds, as listed in <i>Table 1</i> .
RUN	Run Control Input for the Controller. Forcing the RUN pin below 1.1V disables control, while forcing the RUN pin below 0.7V shuts down the entire LTC7897, reducing quiescent current to approximately 1 $\mu$ A. Tie the RUN pin to V <sub>IN</sub> for always-on operation.
GND (EPAD)	Ground (Exposed Pad). The exposed pad must be soldered to PCB GND for rated electrical and thermal performance.
	DRVUV

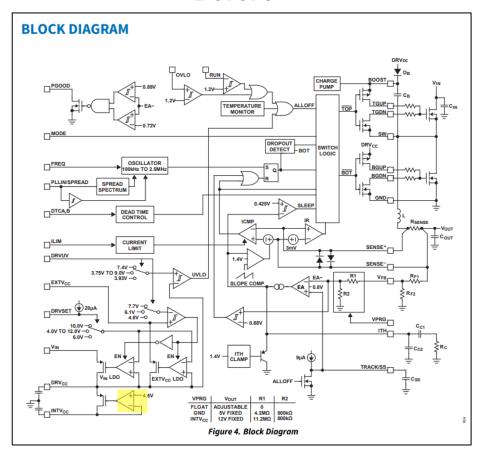
Techdoc: change from 10.0V to 9.7V

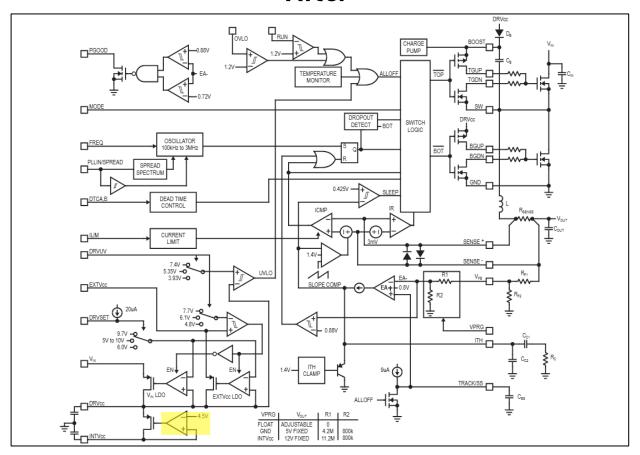
analog.com Rev. A | 12 of 52



▶ Updated Figure 4.

## **Before**

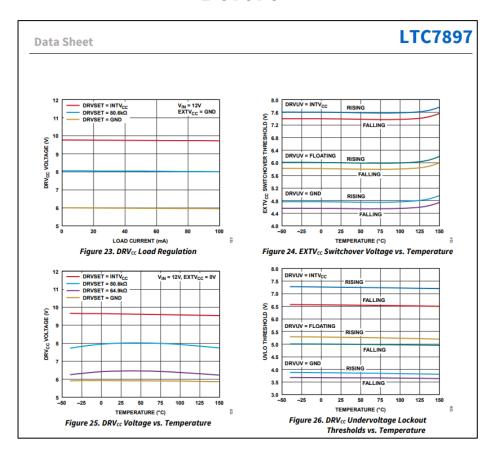


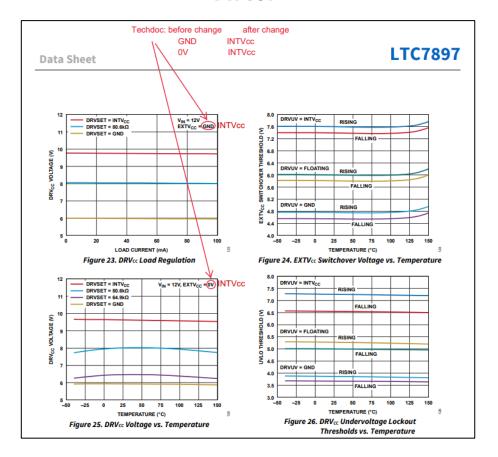




▶ Corrected EXTVcc pin condition setting for Figures 23 and 25.

#### **Before**



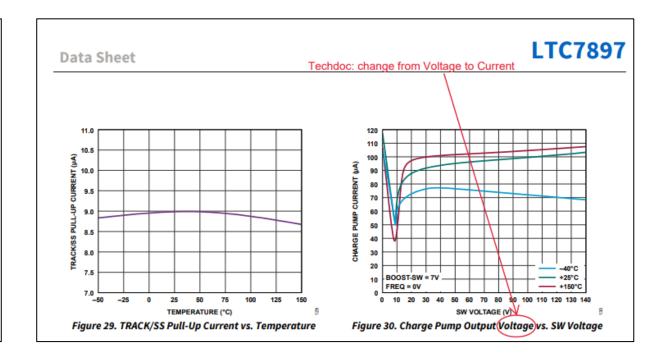




▶ Fixed figure description title for Figure 30.

#### **Before**

# Data Sheet LTC7897 LTC7897





▶ Update DRVcc condition.

#### **Before**

Data Sheet LTC7897

The DRVSET pin programs the DRV $_{\rm CC}$  supply voltage, and the DRVUV pin selects the different DRV $_{\rm CC}$  UVLO and EXTV $_{\rm CC}$  switchover threshold voltages. *Table 6* summarizes the different DRVSET pin configurations along with the voltage settings that go with each configuration. *Table 7* summarizes the different DRVUV pin configurations and voltage settings. Tying the DRVSET pin to INTV $_{\rm CC}$  programs DRV $_{\rm CC}$  to 10V. Tying the DRVSET pin to GND programs DRV $_{\rm CC}$  to 6V. Place a 50k to 100k resistor between DRVSET and GND to program the DRV $_{\rm CC}$  voltage between 5V to 10V, as shown in *Figure 48*.

Table 6. DRVSET Pin Configurations and Voltage Settings

DRVSET PIN	DRV <sub>cc</sub> VOLTAGE (V)
GND	6
INTV <sub>CC</sub>	9.7
Resistor to GND $50k\Omega$ to $100k\Omega$	5 to 10

#### **After**

Data Sheet Techdoc: change 10V to 9.7V LTC7897

The DRVSET pin programs the DRV $_{cc}$  supply voltage, and the DRVUV pin selects the different DRV $_{cc}$  UVLO and EXTV $_{cc}$  switchover threshold voltages. *Table 6* summarizes the different DRVSET pin configurations along with the voltage settings that go with each configuration. *Table 7* summarizes the different DRVUV pin configurations and voltage settings. Tying the DRVSET pin to INTV $_{cc}$  programs DRV $_{cc}$  to (10V). Tying the DRVSET pin to GND programs DRV $_{cc}$  to (10V). Place a 50k to 100k resistor between DRVSET and GND to program the DRV $_{cc}$  voltage between 5V to 10V, as shown in *Figure 48*.

Table 6. DRVSET Pin Configurations and Voltage Settings

DRV <sub>cc</sub> VOLTAGE (V)
6
9.7
5 to 10



Revised text in relation to EXTVcc pin setting.

#### **Before**

Data Sheet LTC7897

To prevent the junction temperature from exceeding the maximum rated as shown in  $Table\ 2$ , check the input supply current while operating in continuous conduction mode (MODE = INTV<sub>CC</sub>) at maximum  $V_{IN}$ .

When the voltage applied to EXTV<sub>CC</sub> rises above its rising switchover threshold, the V<sub>IN</sub> LDO regulator turns off and the EXTV<sub>CC</sub> LDO regulator enables. The EXTV<sub>CC</sub> LDO regulator remains on as long as the voltage applied to EXTV<sub>CC</sub> remains above its falling switchover threshold. The EXTV<sub>CC</sub> LDO attempts to regulate the DRV<sub>CC</sub> voltage to the voltage as programmed by the DRVSET pin. Therefore, while EXTV<sub>CC</sub> is less than this voltage, the LDO regulator is in dropout, and the DRV<sub>CC</sub> voltage is approximately equal to EXTV<sub>CC</sub>. When EXTV<sub>CC</sub> is greater than the programmed voltage (up to an absolute maximum of 30V), DRV<sub>CC</sub> is regulated to the programmed voltage. Using the EXTV<sub>CC</sub> LDO regulator allows the MOSFET driver and control power to be derived from one of the switching regulator outputs of the LTC7897 (4.7V  $\leq$  V<sub>OUT</sub>  $\leq$  30V) during normal operation, and from the V<sub>IN</sub> LDO when the output is out of regulation (e.g., start up or short circuit). If more current is required through the EXTV<sub>CC</sub> LDO than is specified, add an external Schottky diode between the EXTV<sub>CC</sub> and DRV<sub>CC</sub> pins. In this case, do not apply more than 15V to the EXTV<sub>CC</sub> pin.

Significant efficiency and thermal gains can be realized by powering  $DRV_{CC}$  from an outpu because the  $V_{IN}$  current resulting from the driver and control currents is scaled by a factor of  $V_{OUT}/(V_{IN} \cdot Efficiency)$ . For 5V to 30V regulator outputs, connect the EXTV<sub>CC</sub> pin to  $V_{OUT}$ . Tying the EXTV<sub>CC</sub> pin to a 12V supply reduces the junction temperature in Equation 22 from 150°C to the results given by Equation 25, as follows:

$$T_1 = 70^{\circ}\text{C} + (39\text{mA})(12\text{V})(43^{\circ}\text{C/W}) = 90^{\circ}\text{C}$$
 (25)

However, for 3.3V and other low voltage outputs, additional circuitry is required to derive  $DRV_{CC}$  power from the output.

The following list summarizes the four possible connections for EXTV<sub>CC</sub>:

- EXTV<sub>CC</sub> grounded. This connection causes the V<sub>IN</sub> LDO regulator to power DRV<sub>CC</sub>, resulting in an efficiency penalty of up to 10% or more at high input voltages.
- EXTV<sub>CC</sub> connected directly to the regulator output. This connection is the normal connection for an application with an output range of 5V to 30V and provides the highest efficiency.
- EXTV<sub>CC</sub> connected to an external supply. If an external supply is available, it can be used to power EXTV<sub>CC</sub>,
  provided that it is compatible with the MOSFET gate drive requirements. This supply can be higher or lower
  than V<sub>IN</sub>. However, a lower EXTV<sub>CC</sub> voltage results in higher efficiency.
- EXTV<sub>CC</sub> connected to an output derived boost or charge pump. For regulators where outputs are below 5V,
  efficiency gains can still be realized by connecting EXTV<sub>CC</sub> to an output derived voltage that is boosted to
  greater than the EXTV<sub>CC</sub> switchover threshold.

#### **After**

Techdoc: before change after change
15V 14V
outpu output
connected to INTVcc

LTC7897

To prevent the junction temperature from exceeding the maximum rated as shown in *Table 2*, check the input supply current while operating in continuous conduction mode (MODE=INTV<sub>cc</sub>) at maximum  $V_{IN}$ .

When the voltage applied to EXTV<sub>CC</sub> rises above its rising switchover threshold, the V<sub>IN</sub> LDO regulator turns off and the EXTV<sub>CC</sub> LDO regulator enables. The EXTV<sub>CC</sub> LDO regulator remains on as long as the voltage applied to EXTV<sub>CC</sub> remains above its falling switchover threshold. The EXTV<sub>CC</sub> LDO attempts to regulate the DRV<sub>CC</sub> voltage to the voltage as programmed by the DRVSET pin. Therefore, while EXTV<sub>CC</sub> is less than this voltage, the LDO regulator is in dropout, and the DRV<sub>CC</sub> voltage is approximately equal to EXTV<sub>CC</sub>. When EXTV<sub>CC</sub> is greater than the programmed voltage (up to an absolute maximum of 30V), DRV<sub>CC</sub> is regulated to the programmed voltage. Using the EXTV<sub>CC</sub> LDO regulator allows the MOSFET driver and control power to be derived from one of the switching regulator outputs of the LTC7897 (4.7V  $\leq$  V<sub>OUT</sub>  $\leq$  30V) during normal operation, and from the V<sub>IN</sub> LDO when the output is out of regulation (e.g., start up or short circuit). If more current is required through the EXTV<sub>CC</sub> LDO than is specified, add an external Schottky diode between the EXTV<sub>CC</sub> and DRV<sub>CC</sub> pins. In this case, do not apply more than (5) to the EXTV<sub>CC</sub> pin.

Significant efficiency and thermal gains can be realized by powering DRV<sub>CC</sub> from an outpubecause the  $V_{IN}$  current resulting from the driver and control currents is scaled by a factor of  $V_{OUT}/(V_{IN} \cdot Efficiency)$ . For 5V to 30V regulator outputs, connect the EXTV<sub>CC</sub> pin to  $V_{OUT}$ . Tying the EXTV<sub>CC</sub> pin to a 12V supply reduces the junction temperature in Equation 22 from 150°C to the results given by Equation 25, as follows:

$$T_1 = 70^{\circ}\text{C} + (39\text{mA})(12\text{V})(43^{\circ}\text{C/W}) = 90^{\circ}\text{C}$$
 (25)

However, for 3.3V and other low voltage outputs, additional circuitry is required to derive DRV<sub>cc</sub> power from the output.

The following list summarizes the four possible connections for EXTV<sub>CC</sub>:

- EXTV<sub>cc</sub> grounded. This connection causes the V<sub>IN</sub> LDO regulator to power DRV<sub>cc</sub>, resulting in an efficiency penalty of up to 10% or more at high input voltages.
- EXTV<sub>CC</sub> connected directly to the regulator output. This connection is the normal connection for an application with an output range of 5V to 30V and provides the highest efficiency.
- EXTV<sub>CC</sub> connected to an external supply. If an external supply is available, it can be used to power EXTV<sub>CC</sub>,
  provided that it is compatible with the MOSFET gate drive requirements. This supply can be higher or lower
  than V<sub>IN</sub>. However, a lower EXTV<sub>CC</sub> voltage results in higher efficiency.
- EXTV<sub>CC</sub> connected to an output derived boost or charge pump. For regulators where outputs are below 5V,
  efficiency gains can still be realized by connecting EXTV<sub>CC</sub> to an output derived voltage that is boosted to
  greater than the EXTV<sub>CC</sub> switchover threshold.



Update minimum on time values.

#### **Before**

Data Sheet LTC7897

#### **Minimum On-Time Considerations**

The minimum on-time  $(t_{ON(MIN)})$  is the smallest time duration that the LTC7897 is capable of turning on the top MOSFET.  $t_{ON(MIN)}$  is determined by internal timing delays and the gate charge required to turn on the MOSFET. Low duty cycle applications can approach this minimum on-time limit. Take care to ensure the results in Equation 26, as follows:

$$t_{ON(MIN)} < \frac{V_{OUT}}{V_{IN'f}} \tag{26}$$

If the duty cycle falls below what can be accommodated by the minimum on time, the controller begins to skip cycles. The output voltage continues to be regulated, but the ripple voltage and current increase. The minimum on time for the LTC7897 is approximately 60ns. However, as the peak sense voltage decreases, the minimum on time gradually increases up to about 80ns. This change is of particular concern in forced continuous applications with low ripple current at light loads. If the duty cycle drops below the minimum on-time limit in this situation, a significant amount of cycle skipping can occur with correspondingly larger current and voltage ripple.

#### **Fault Conditions: Current Limit and Foldback**

The LTC7897 includes current foldback to reduce the load current when the output is shorted to GND. If the output voltage falls below 70% of its regulation point, the maximum sense voltage is progressively lowered from 100% to 40% of its maximum value. Under short-circuit conditions with low duty cycles, the LTC7897 begins cycle skipping to limit the short-circuit current. In this situation, the bottom MOSFET dissipates most of the power, but less than in normal operation. The short-circuit ripple current ( $\Delta I_{L(SC)}$ ) is determined by  $t_{ON(MIN)} \approx 60$ ns, the input voltage, and the inductor value given by Equation 27, as follows:

$$\Delta I_{L(SC)} = t_{ON(MIN)} \cdot V_{IN}/L \tag{27}$$

The resulting average short-circuit current (I<sub>SC</sub>) is given by Equation 28, as follows:

$$I_{SC} = 40\% \cdot I_{LIM(MAX)} - \frac{\Delta I_{L(SC)}}{2}$$
(28)

where ILIM(MAX) is the maximum peak inductor current.

#### **After**

	Techdoc: before change	after change	
	60	80	
	80	100	LTC7897
Data Sheet	60	80	LICIOSI

#### **Minimum On-Time Considerations**

The minimum on-time  $(t_{ON(MIN)})$  is the smallest time duration that the LTC7897 is capable of turning on the top MOSFET.  $t_{ON(MIN)}$  is determined by internal timing delays and the gate charge required to turn on the MOSFET. Low duty cycle applications can approach this minimum on-time limit. Take care to ensure the results in Equation 26, as follows:

$$t_{ON(MIN)} < \frac{v_{OUT}}{v_{In} \cdot f}$$
(26)

If the duty cycle falls below what can be accommodated by the minimum on time, the controller begins to skip cycles. The output voltage continues to be regulated, but the ripple voltage and current increase. The minimum on time for the LTC7897 is approximately 60ns. However, as the peak sense voltage decreases, the minimum on time gradually increases up to about 60ns. This change is of particular concern in forced continuous applications with low ripple current at light loads. If the duty cycle drops below the minimum on-time limit in this situation, a significant amount of cycle skipping can occur with correspondingly larger current and voltage ripple.

#### Fault Conditions: Current Limit and Foldback

The LTC7897 includes current foldback to reduce the load current when the output is shorted to GND. If the output voltage falls below 70% of its regulation point, the maximum sense voltage is progressively lowered from 100% to 40% of its maximum value. Under short-circuit conditions with low duty cycles, the LTC7897 begins cycle skipping to limit the short-circuit current. In this situation, the bottom MOSFET dissipates most of the power, but less than in normal operation. The short-circuit ripple current ( $\Delta I_{L(SC)}$ ) is determined by  $t_{ON(MIN)} \approx 60$ ns, the input voltage, and the inductor value given by Equation 27, as follows:

$$\Delta I_{L(SC)} = t_{ON(MIN)} \cdot V_{IN}/L \tag{27}$$

The resulting average short-circuit current (I<sub>SC</sub>) is given by Equation 28, as follows:

$$I_{SC} = 40\% \cdot I_{LIM(MAX)} - \frac{\Delta I_{L(SC)}}{2}$$
(28)

where ILIM(MAX) is the maximum peak inductor current.



▶ Updated text from Efficiency Considerations section.

#### **Before**

Data Sheet LTC7897

Other hidden losses, such as copper trace and internal battery resistances, can account for an additional 5% to 10% efficiency degradation in portable systems. It is important to include these system level losses during the design phase. The internal battery and fuse resistance losses can be minimized by making sure that  $C_{IN}$  has adequate charge storage and low ESR at the switching frequency. A 25W supply typically requires a minimum of  $20\mu F$  to  $40\mu F$  of capacitance with a maximum of  $20m\Omega$  to  $50m\Omega$  of ESR. Other losses, including inductor core losses, generally account for less than 2% of the total additional loss. Other losses, including inductor core losses, generally account for less than 2% of the total additional loss.

#### After

Techdoc: remove this sentence.

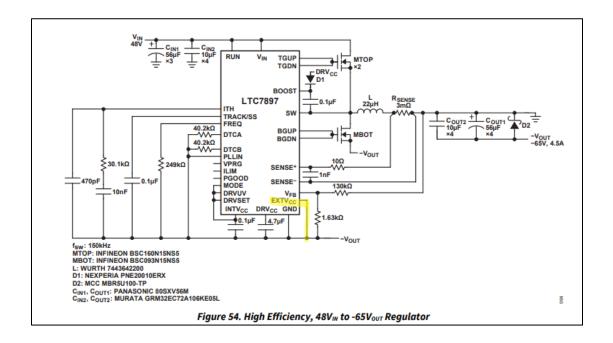
LTC7897

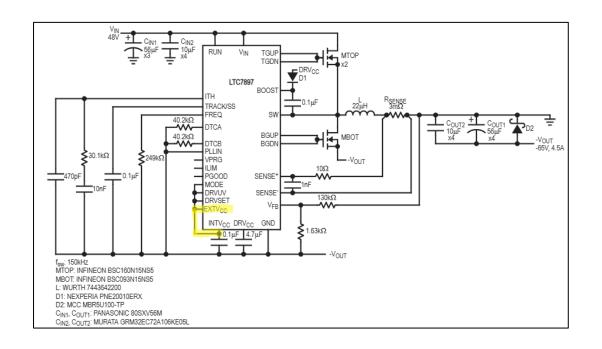
Other hidden losses, such as copper trace and internal battery resistances, can account for an additional 5% to 10% efficiency degradation in portable systems. It is important to include these system level losses during the design phase. The internal battery and fuse resistance losses can be minimized by making sure that  $C_{IN}$  has adequate charge storage and low ESR at the switching frequency. A 25W supply typically requires a minimum of  $20\mu F$  to  $40\mu F$  of capacitance with a maximum of  $20m\Omega$  to  $50m\Omega$  of ESR. Other losses, including inductor core losses, generally account for less than 2% of the total additional loss. Other losses, including inductor core losses, generally account for less than 2% of the total additional loss.



▶ Updated Figure 54.

### **Before**







▶ Updated Figure 58.

#### **Before**

